

# Minimising sludge production by long SRT, trash and grit removal from sludge

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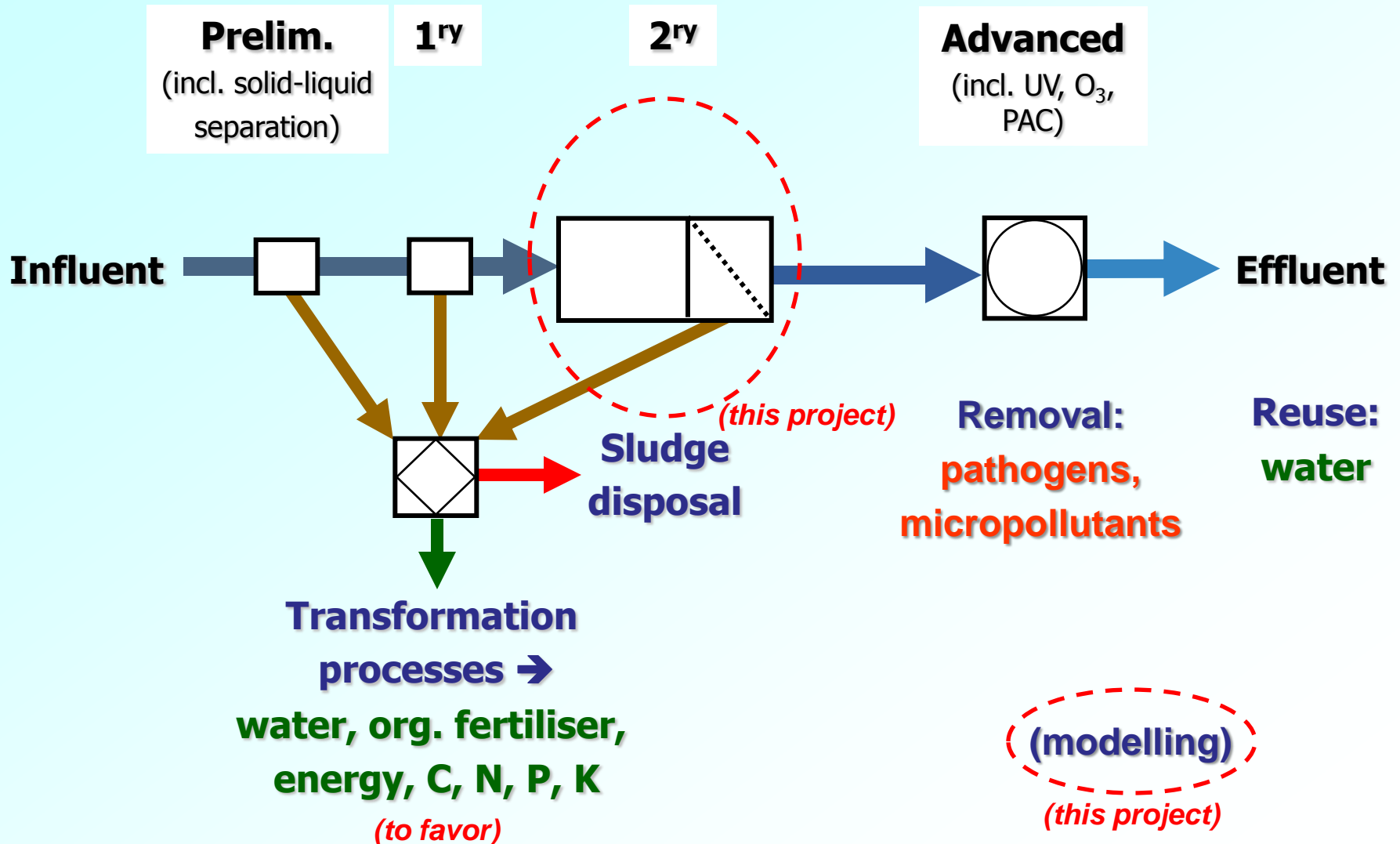
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# Outline

- **WWT & sludge production**
- **Modelling sludge production**
- **Objectives**
- **Experimental units**
- **Trash and grit removal**
- **Biodegradation of « unbiodegradables »**
- **Conclusions and Perspectives**

# Wastewater Treatment (or WW Resource Management)



# Costs of WWT

Effect (+: **positive**/-: **negative**)  
of reducing sludge production

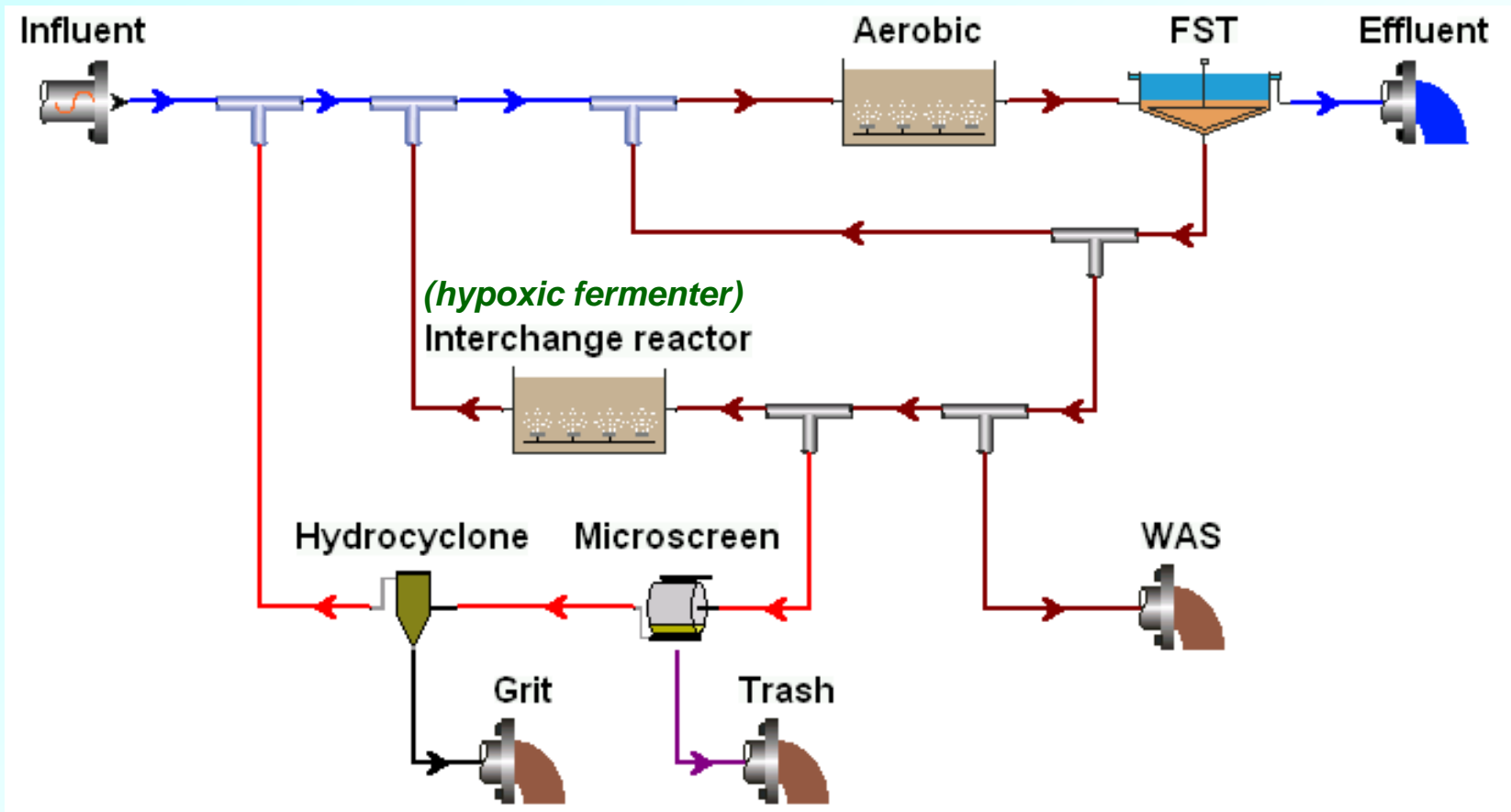
- **Capital costs:**
  - + **size of bioreactors, settling tanks, sludge treatment units**
- **Operating costs:**
  - **aeration**
  - + **sludge treatment & disposal**
    - increasing sludge disposal costs
      - Quebec: from 20 to >80 \$/wet t. from 2000 to 2009

# Reducing sludge production

- Chemical: ozonation, uncoupling
- Thermal: thermal disruption
- Physical: mechanical disruption, ultrasounds, pressure drop, **microscreening, hydrocycloning**
- Biological: predation, anaerobic digestion, **fermentation, endogenous respiration (SRT)**

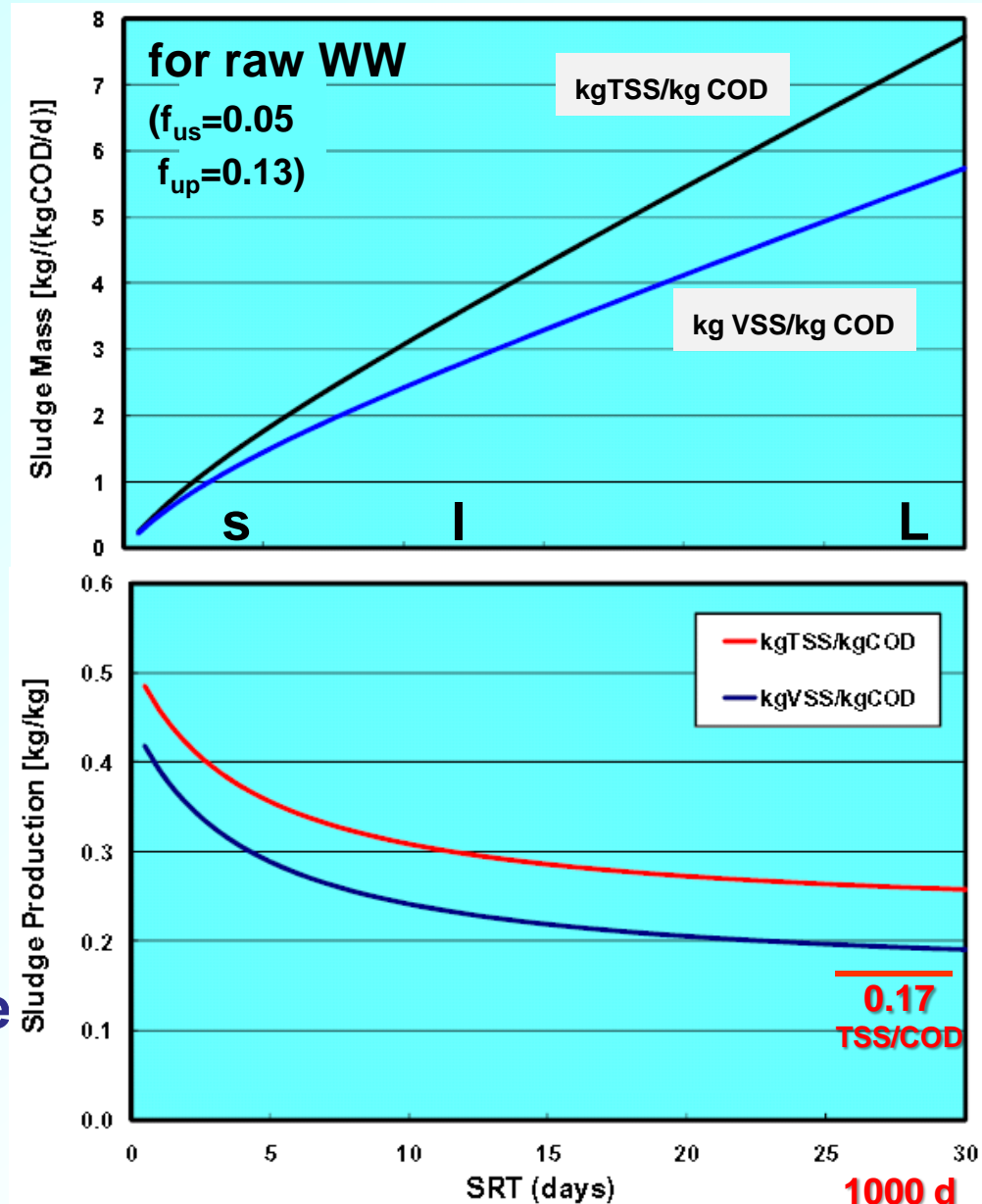
# Cannibal<sup>®</sup>

- Claims of « no » or minimal sludge production
- Limited data available – How does it work?

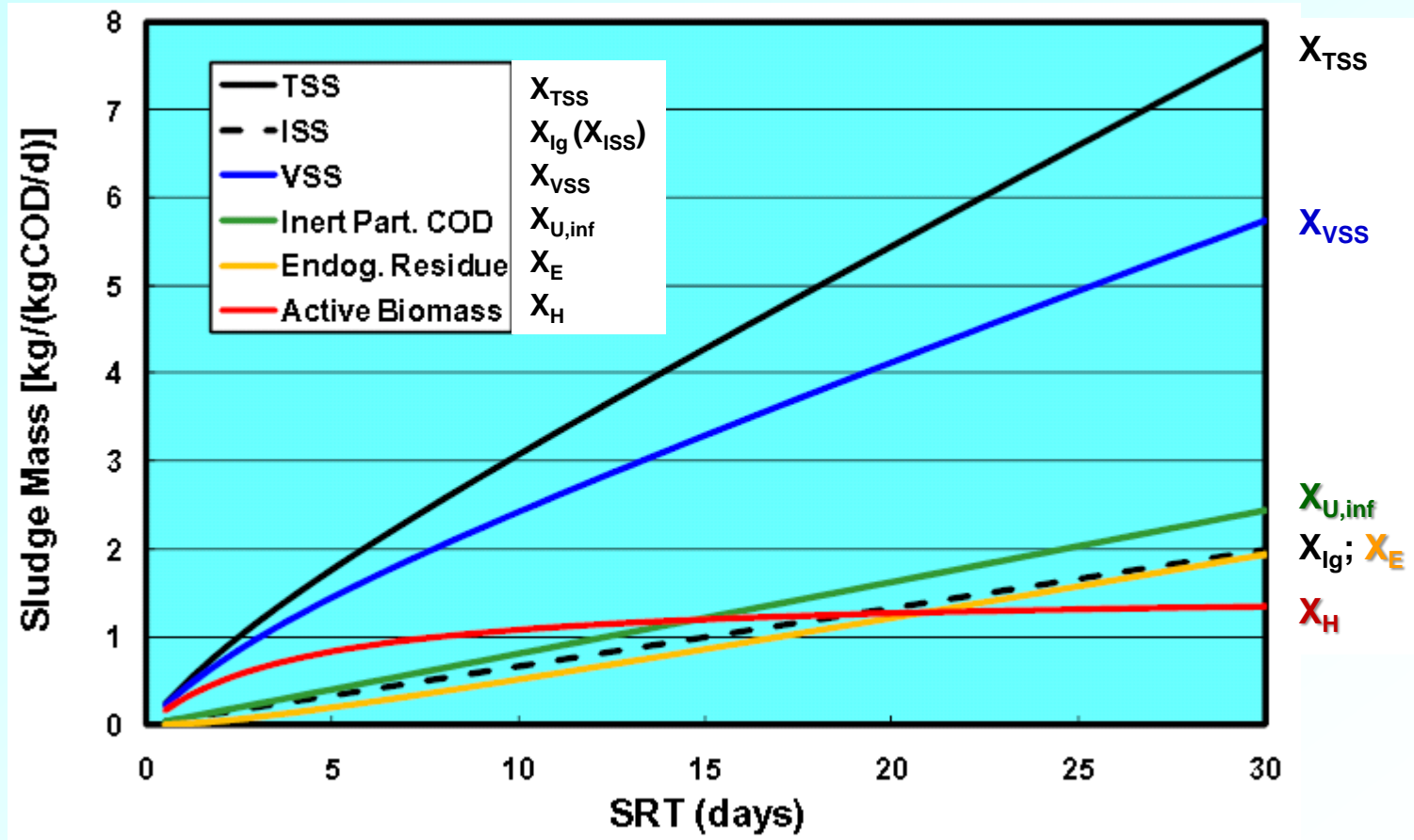


# Sludge reduction: Effect of SRT

- Short SRT for BOD removal
- Longer SRT for N and P removal at cold temperature
- Longest SRT for small-medium WWTPs to minimize sludge production (but increased costs of aeration)  
e.g. SRT 5 d to 30 d → **25%** less kg TSS/kg COD
- Thus, long SRT → low sludge production (WAS + effluent) (nothing magical)



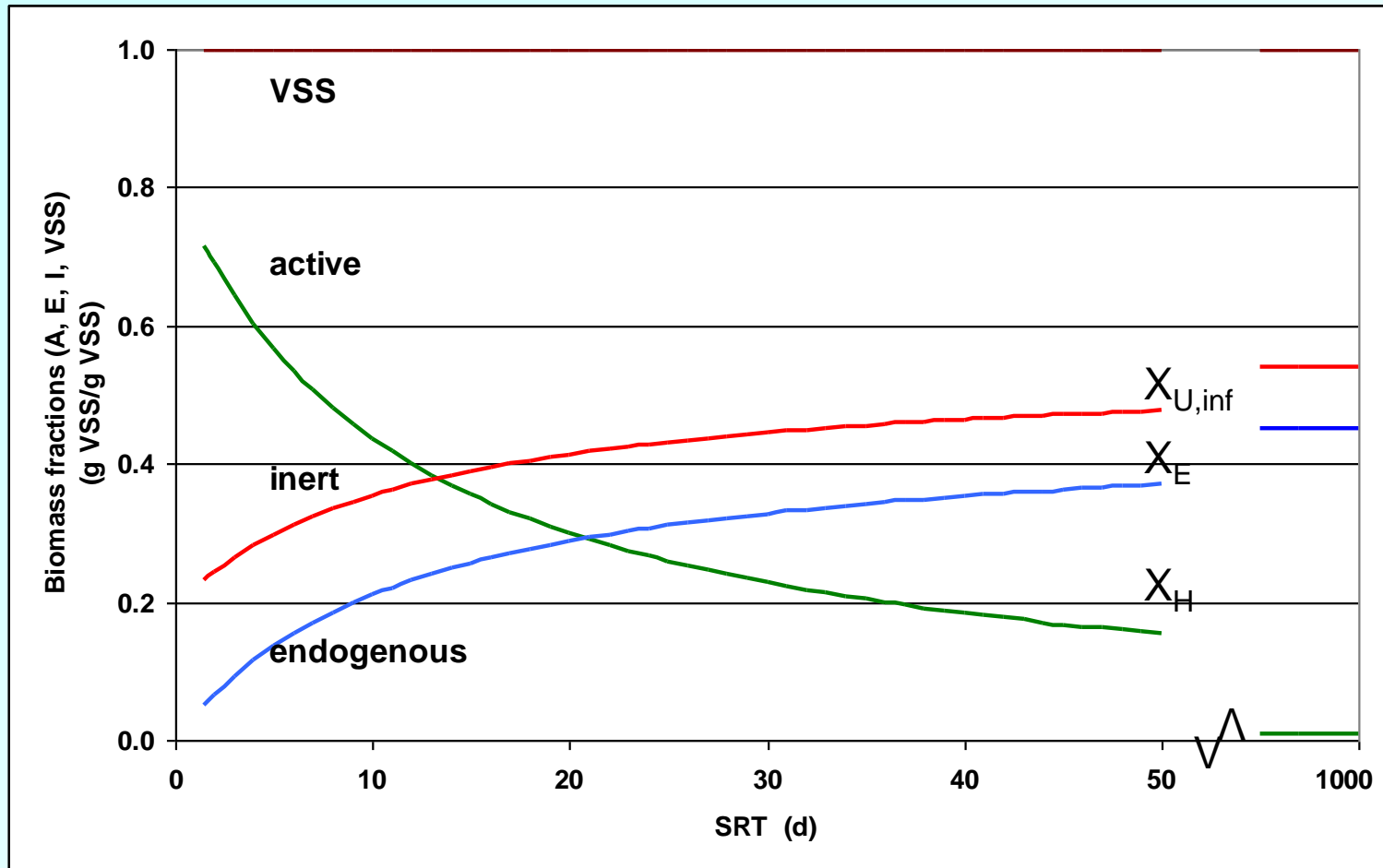
# Mixed liquor components vs SRT



with increasing SRT, leveling of  $X_H$   
 but continuous increase in  $X_{Ig}$ ,  $X_{U,inf}$ ,  $X_E$



# MLVSS fractions vs SRT

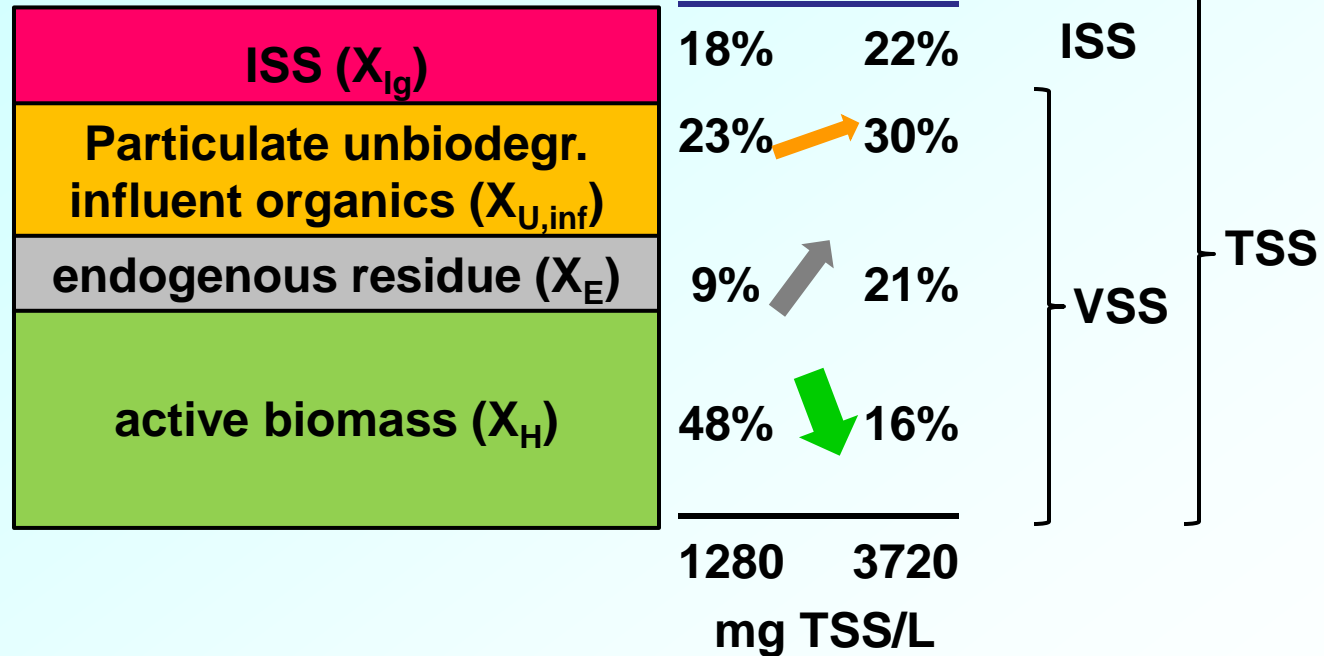


- at very high SRTs, the active biomass fraction becomes minimal and the VSS are essentially composed of  $X_{U,inf}$  and  $X_E$

# Mixed liquor composition

SRT

5 d      20 d



Example:  
raw WW: 280 mg COD/L  
aerobic AS, 20°C, 8 h HRT

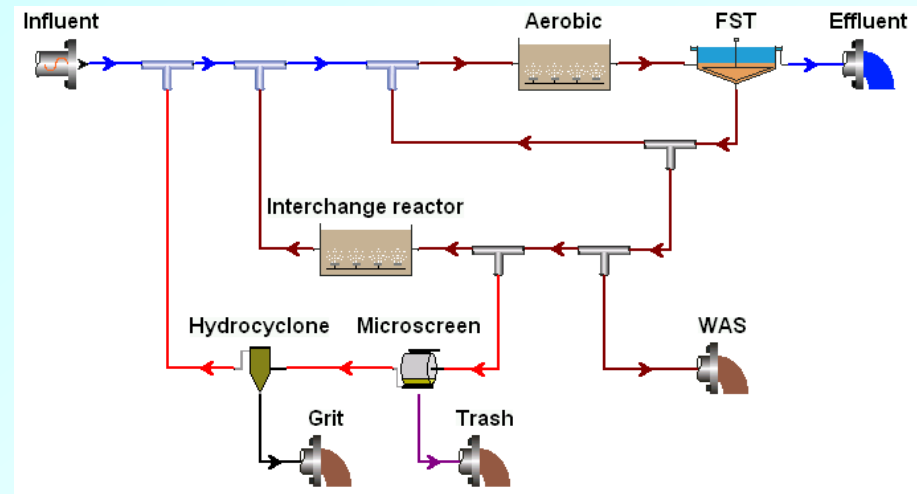
→ from 5 to 20 d SRT, 2.9 times more sludge (but 3x less  $X_H$ )

→ if 33% removal of grit (in  $X_{Ig}$ ) and of trash (in  $X_{U,inf}$ ) can be removed from sludge at an SRT of 20 d, the capacity can be increased by 17% (7+10)

→ treatment capacity increased or reduced reactor size

# Cannibal®

## Research questions



- Can grit ( $X_{I_g}$ ) and trash ( $X_{U,inf}$ ) removal from the mixed liquor be efficiently removed enough to increase significantly the treatment plant capacity?
  - what is the effect on sludge settleability?
- Can « unbiodegradable »  $X_E$  (endog. residue) and  $X_{U,inf}$  (infl. partic. unbiodeg. org.) be biodegraded at long SRTs and in the AN/ox fermentation reactor?
  - can the lower sludge production savings compensate the extra aeration costs?

# Objectives

« Explain » the Cannibal<sup>®</sup> process by:

1) Modelling biological and unit processes

**Characterizing the efficiency of:**

2) physical removal from mixed liquor (or RAS) by:

2.1 microscreening (MS) of trash ( $X_{U,inf}$ )

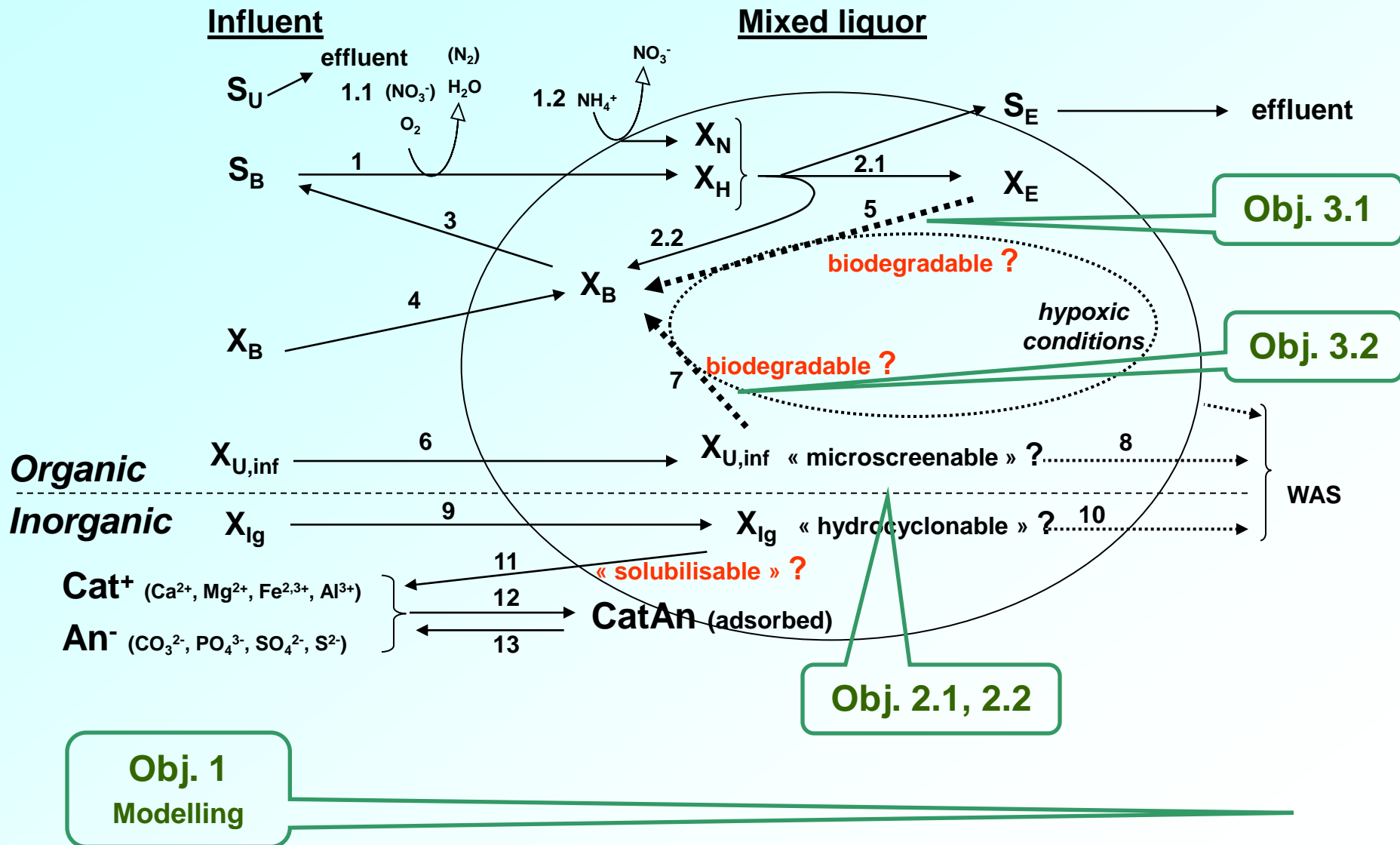
2.2 hydrocycloning (HC) of grit ( $X_{lg}$ )

3) biodegradation of the mixed liquor components:

3.1 endogenous residue ( $X_E$ )

3.2 influent « unbiodegrad. » partic. organics ( $X_{U,inf}$ )

# Processes & objectives

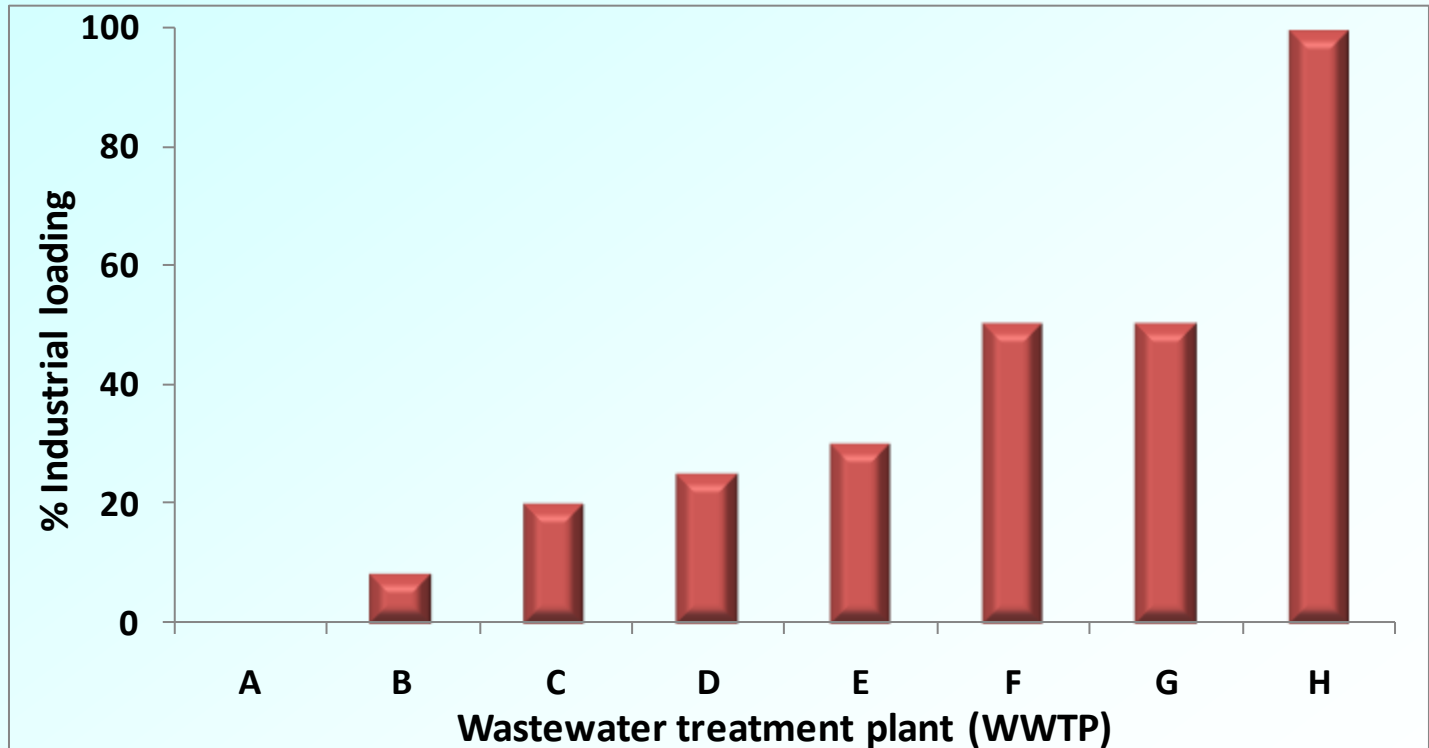


# Methodology

- **Lab tests**
  - MS and HC
  - Biodegradation of  $X_E$
- **Modelling**
- **Pilot testing**

# MS & HC: ML & RAS samples

from 8 WWTPs near Montreal



Preliminary tr.	Coarse screening	✓	✓	✓	✓	✓	✓	✓	✓
	Grit removal		✓				✓	✓	✓
Primary tr.	Clarifier					✓		✓	

8  
4  
2

# Lab scale HC and MS



HC

200 L

Raw  
sludge

Microscreen

Ø: 10 cm  
200, 300 & 500 µm

Screen  
underflow

Screen  
underflow

200 L

Lab floor

Hydrocyclone

Overflow  
160 L

Underflow  
40 L

Pit floor



mixer above MS



Microscreen

ML &  
RAS



# Lab microscreening (MS) of mixed liquor and RAS

Trash (organic) retained by MS:

hygienic paper, vegetal (plants, wood) residues, hair, large filamentous flocs, etc.

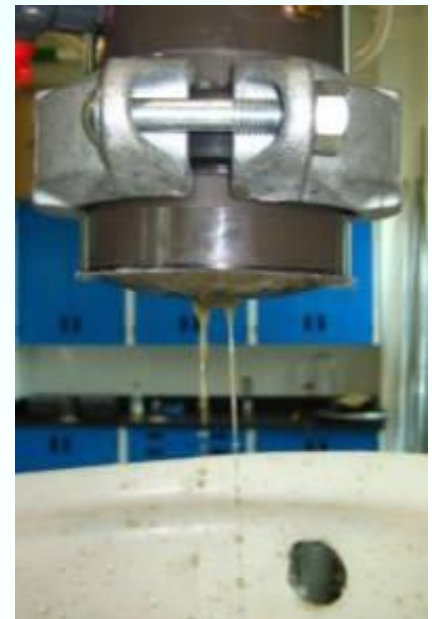
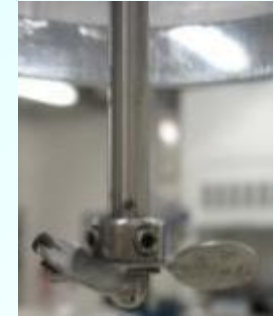
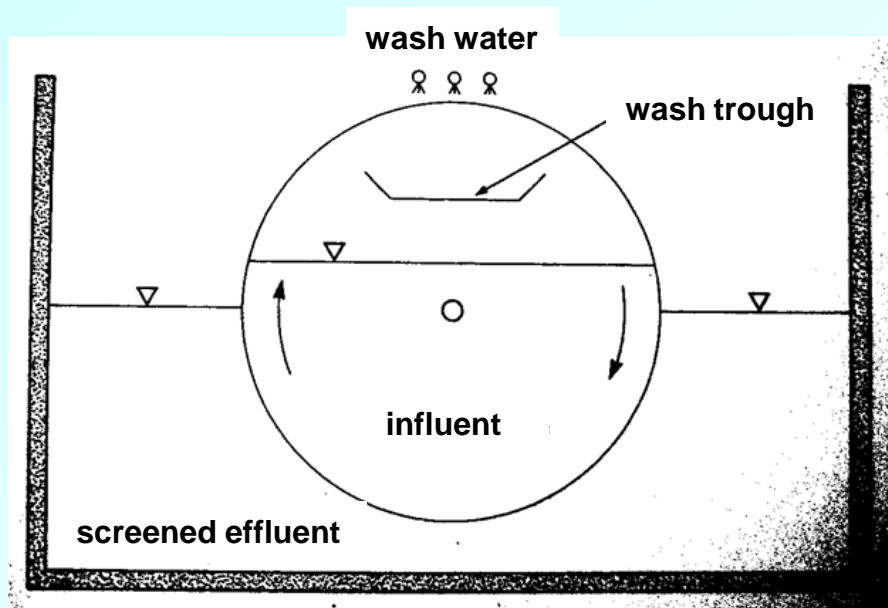


(+ sand)



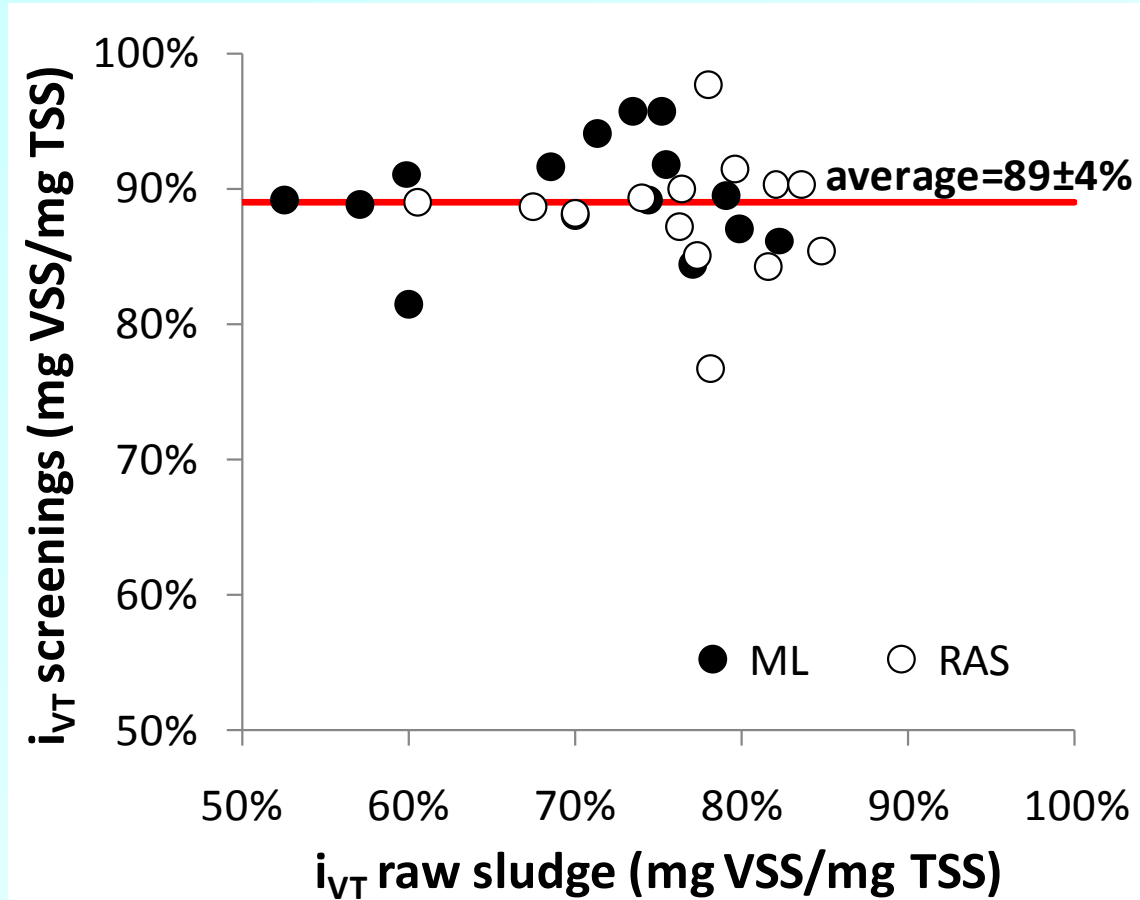
# Microscreen

- Direct removal: by size
- Indirect removal: by dynamic filtration



# Microscreen - results

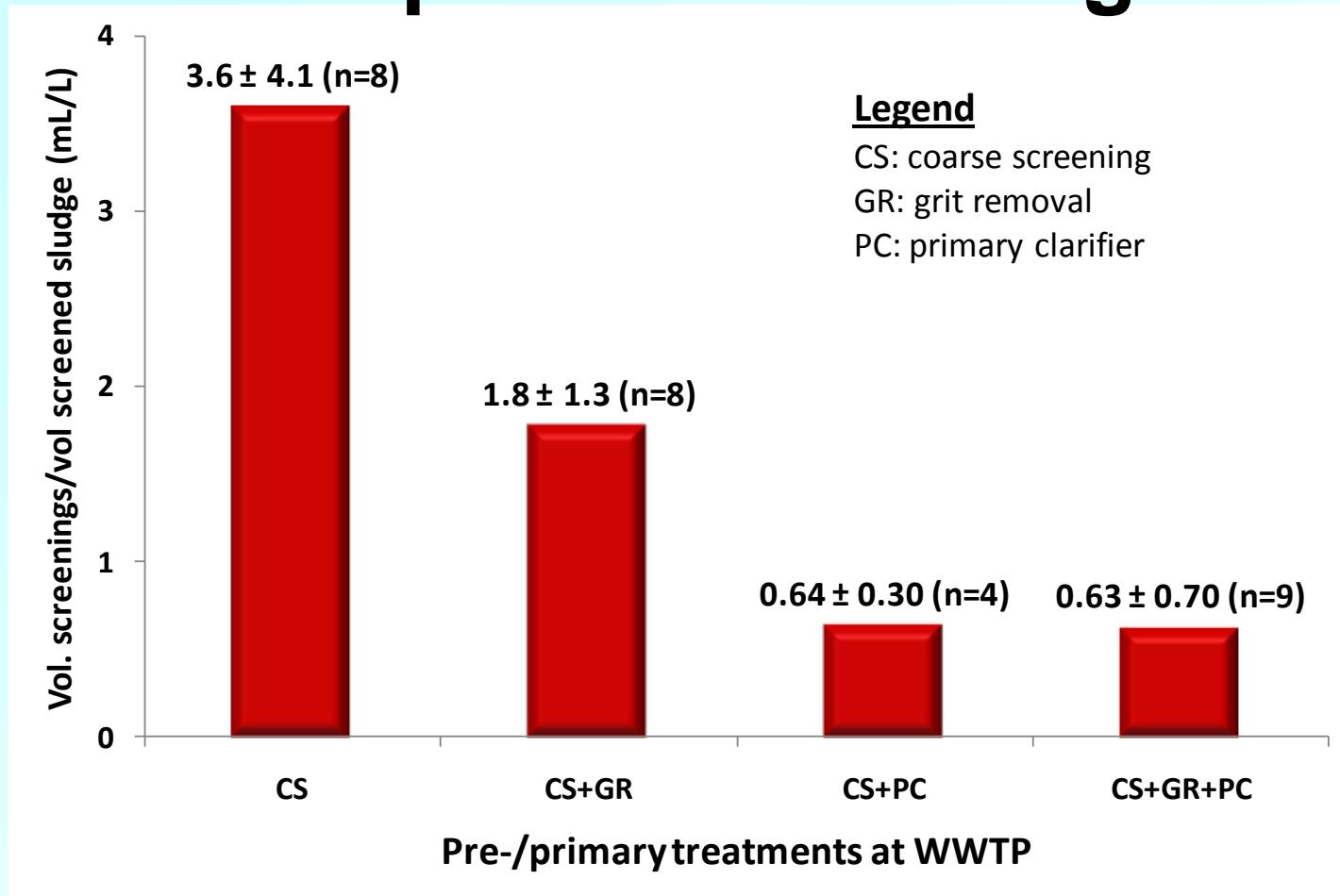
## Effect of raw sludge $i_{VT}$ on screenings $i_{VT}$



vs 99±1% for toilet paper, Kleenex, paper towel

screenings  $i_{VT}$  relatively constant ( $89 \pm 4\%$ ) for ML and RAS  
→ selective removal of organic matter of similar composition is possible

# Effect of WWTP pretreatment on captured screenings



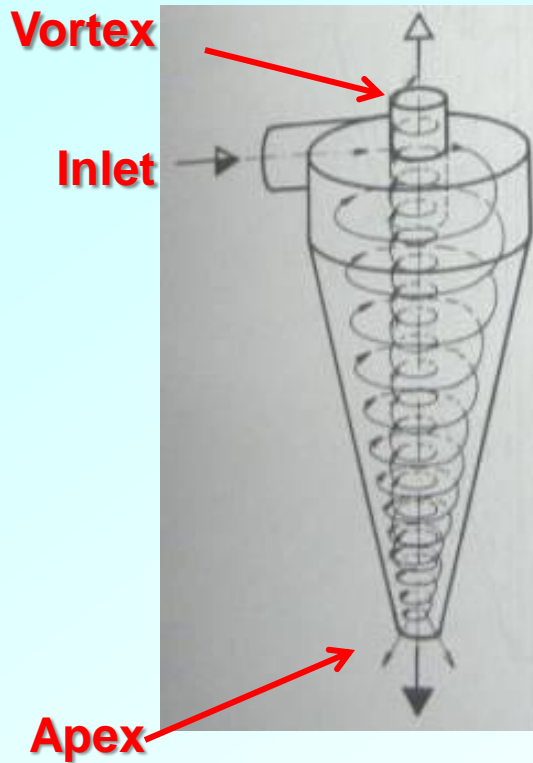
- Improved pretreatment results in less screenings that can be removed from the mixed liquor (or RAS) by MS
- ? g TSS/g COD & ? cost/kg TSS

# Hydrocycloning: grit removal ( $X_{lg}$ ) from mixed liquor and RAS

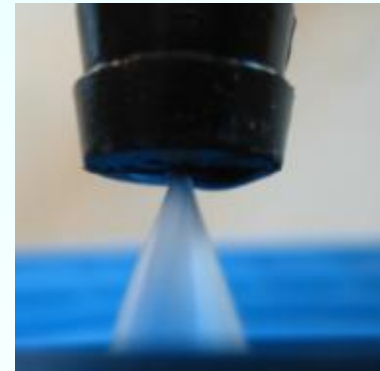
## Composition of $X_{lg}$ :

- inorganics associated to  $X_H$ ,  $X_E$ ,  $X_{U,inf}$  (~9% VSS)
- precipitates (mainly with Al, Fe, Ca)
- **fine sand**, silt, egg shells, etc.

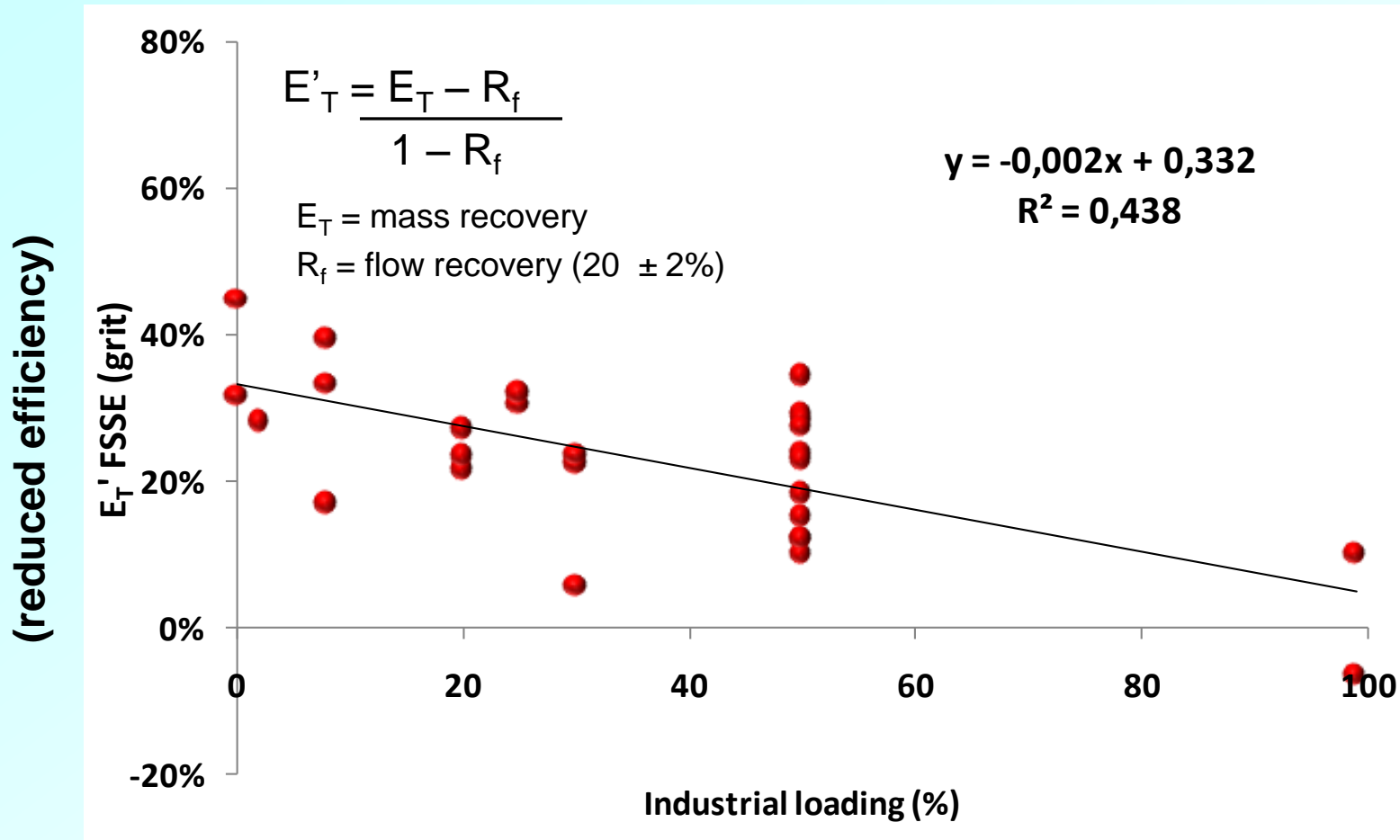
# Hydrocyclone



(Svarovsky, 1984)



# Effect of %industrial loading on $X_{ISS,Inf}$ (FSSE) removal by the HC



- Higher efficiency with a smaller industrial loading:  
→ sand from the municipality, not the industry
- About  $25 \pm 10\%$  of ISS can be removed by HC

# Endogenous residue ( $X_E$ ) biodegradation

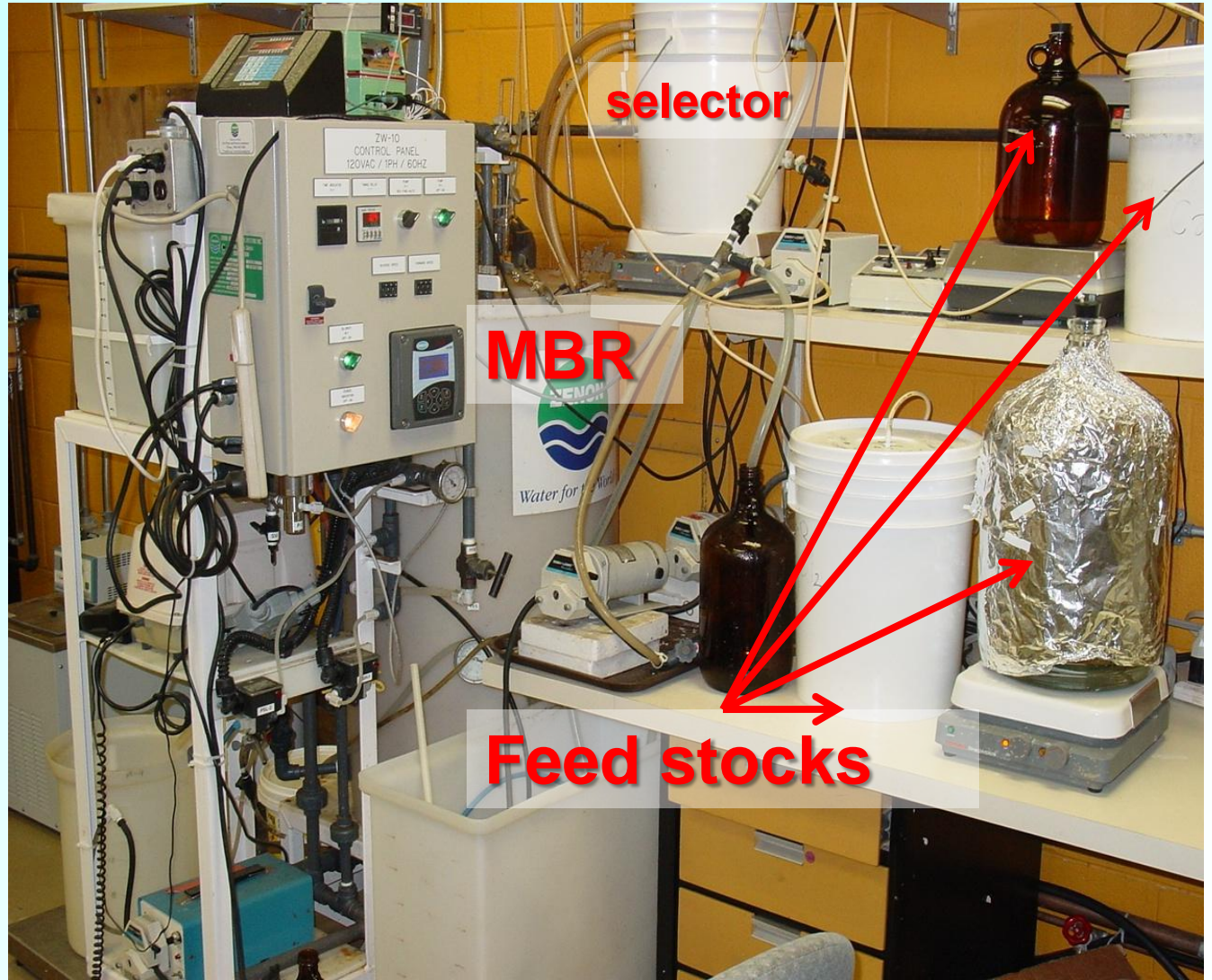
- 1. Production of mixed liquor containing only ( $X_H + X_E$ ) from a synthetic feed with acetate as sole carbon source in an MBR (200 L)**
  - determination of the active fraction ( $F_A$ )
- 2. Mixed liquor biodegradation under**
  - 2.1 anaerobic (AN) conditions**
  - 2.2 anaerobic-aerobic (AN-OX) conditions**



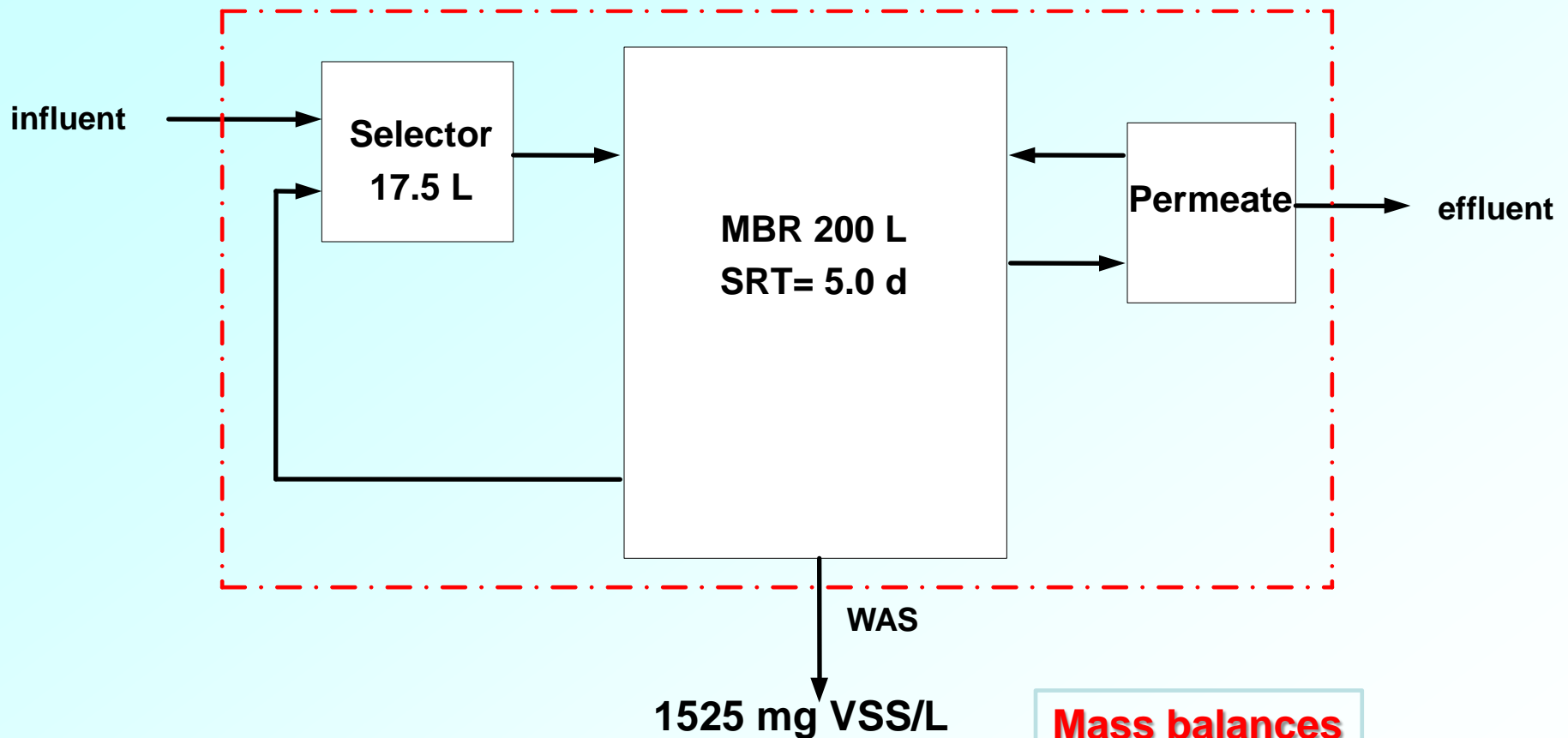
# MBR setup



Zenon hollow fibers (ZW-10, 0.04  $\mu\text{m}$ )



# Removal efficiency and mass balances



## Removal efficiency

COD: > 97%

TKN: > 96%

## Mass balances

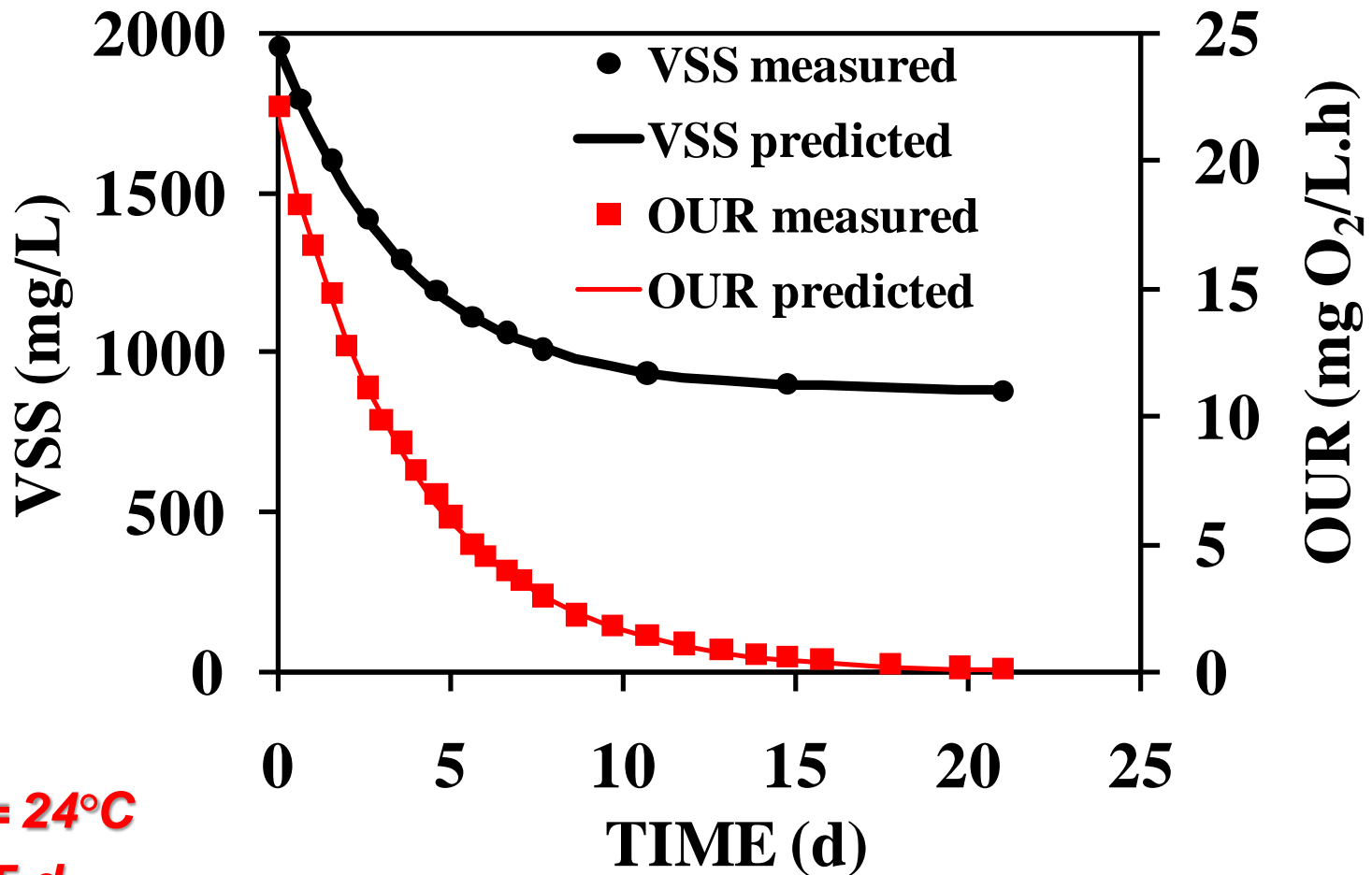
Hydraulic: 99.5 ± 0.4 (%)

COD: 98.4 ± 1.8 (%)

N: 101.9 ± 2.0 (%)

P: 102.8 ± 1.1 (%)

# Active fraction ( $F_A$ ) determination by 21 d endogenous respiration



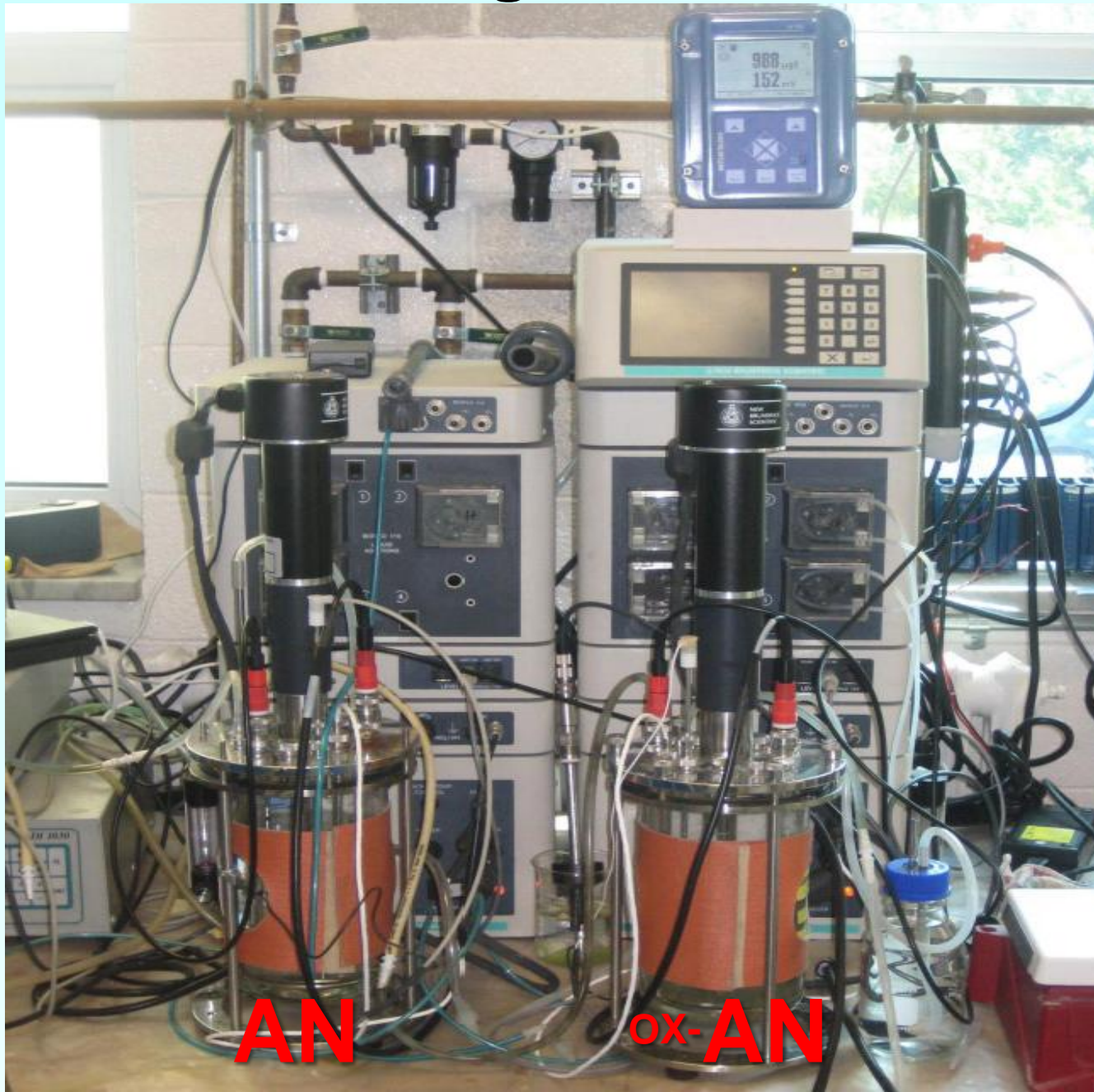
**Temp = 24°C**

**SRT = 5 d**

by VSS:  $b_T = 0.272 \text{ d}^{-1}$  ( $0.243 \text{ d}^{-1}$  @ 20°C);  $F_A = \underline{0.685} \text{ g } X_H/\text{g VSS}$

by OUR.:  $b_T = 0.263 \text{ d}^{-1}$  ( $0.235 \text{ d}^{-1}$  @ 20°C);  $F_A = \underline{0.683} \text{ g } X_H/\text{g VSS}$

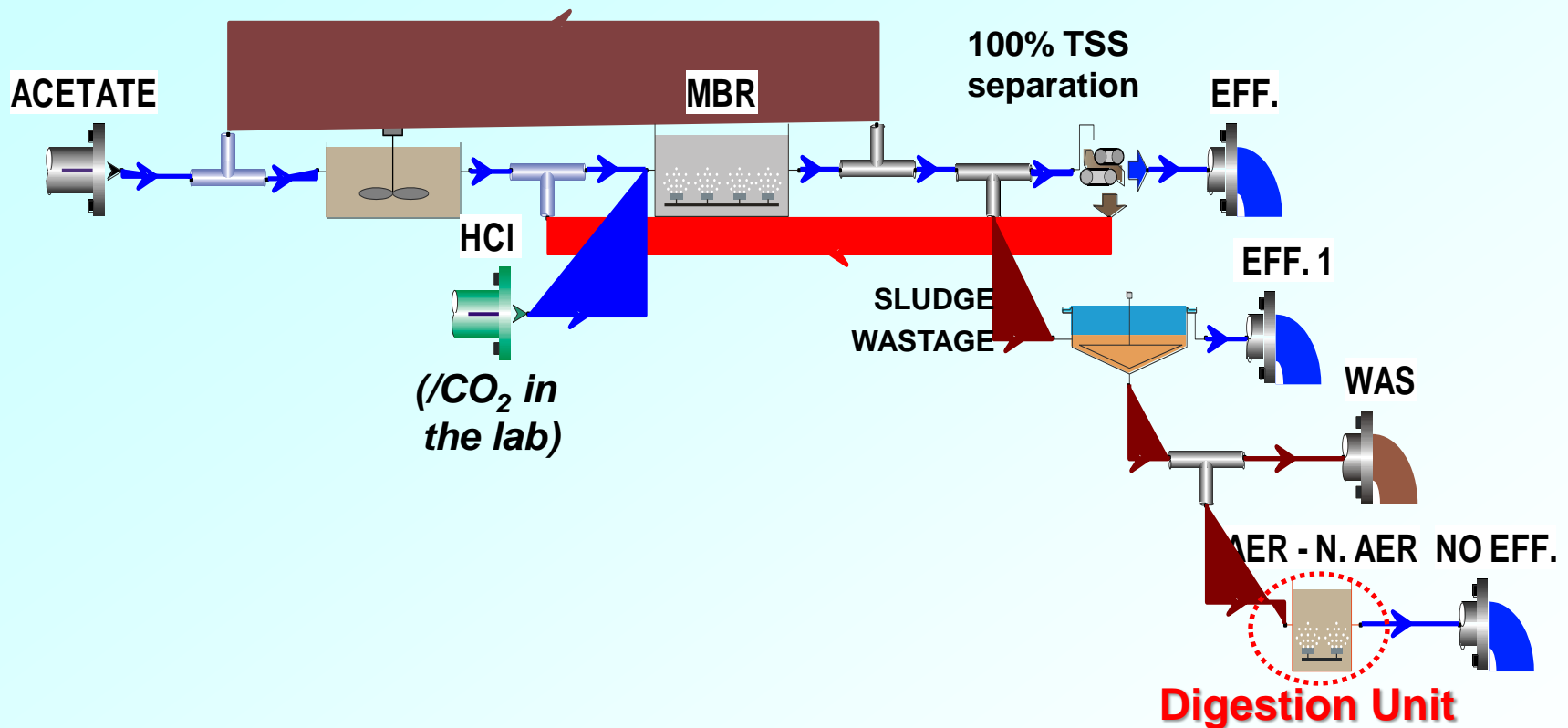
# Batch digestion units



AN

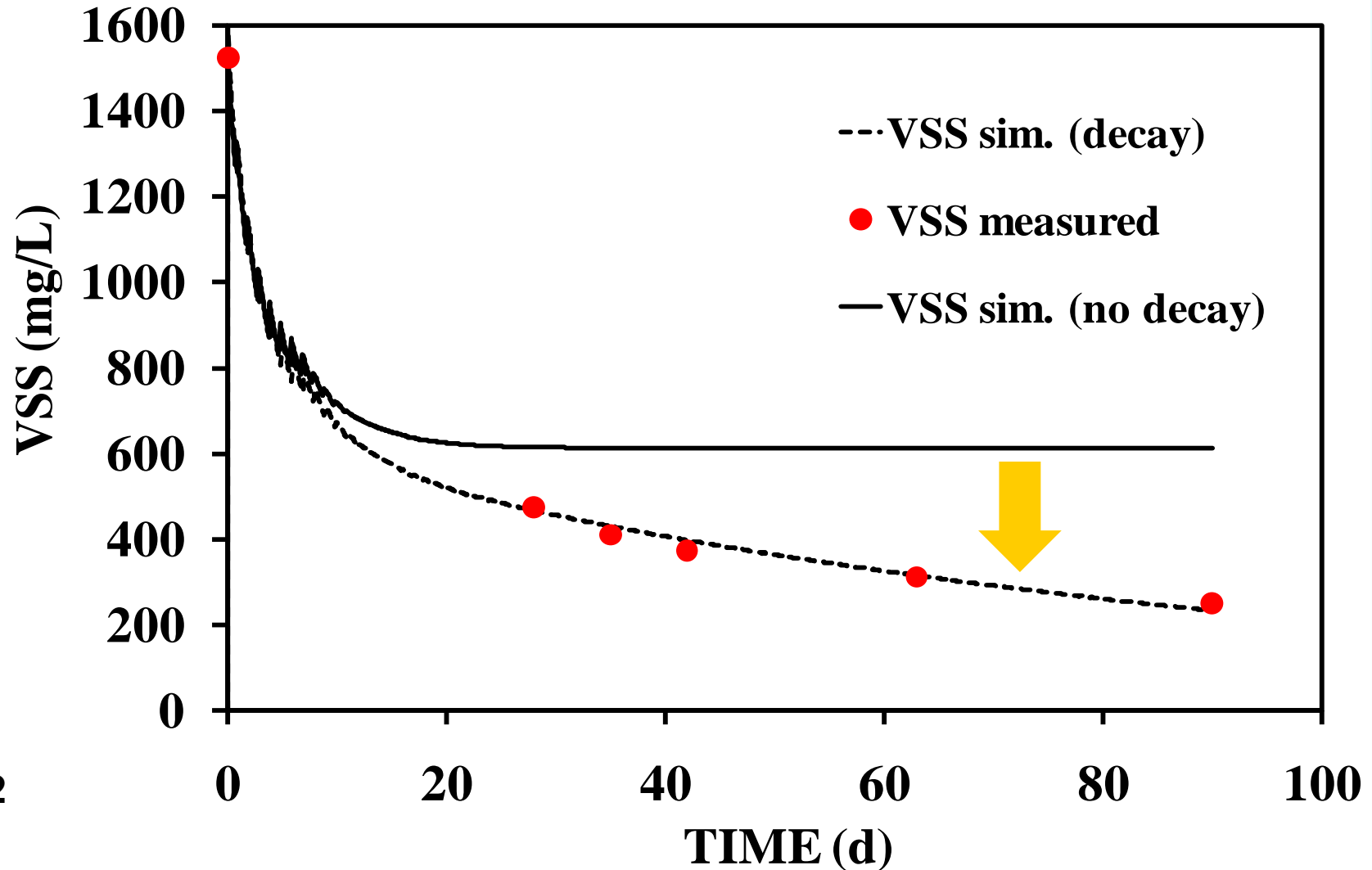
OX-AN

# Modelling with BioWin (OX-AN)



- Simulations consider or not the biodegradation of  $X_E$
- Determination of the rate of  $X_E$  biodegradation:  $k_{d,XE}$

# ML biodegradation tests – AN-OX Results



pH 7.2

AN-OX:  $k_{d,XE,35C,AN-OX} = 0.012 \text{ d}^{-1}$   
(AN:  $k_{d,XE,35C,AN} = 0.005 \text{ d}^{-1}$ )

# Biodegradation of « unbiodegradable » organics

- $X_E$  is very slowly biodegradable
  - more rapid under AN-OX ( $0.012 \text{ d}^{-1}$ ) than AN ( $0.005 \text{ d}^{-1}$ ) conditions at pH 7.2 and  $35^\circ\text{C}$
  - Arrhenius coefficient to determine
- $X_{U,Inf}$  is probably also similarly « slowly biodegradable »

# Demo scale MBR with MS and HC

## ➤ Mobile WWTP unit (16 m long) at St-Hyacinthe WWTP



- Activated sludge basins (1, 3, 5 m<sup>3</sup> + FST)
- MBR (membrane bioreactor – hollow fibers)
- (option: SBR or media for MBBR or IFFAS)

*(Observation: essentially no grit and trash in sludge fed from a primary effluent)*



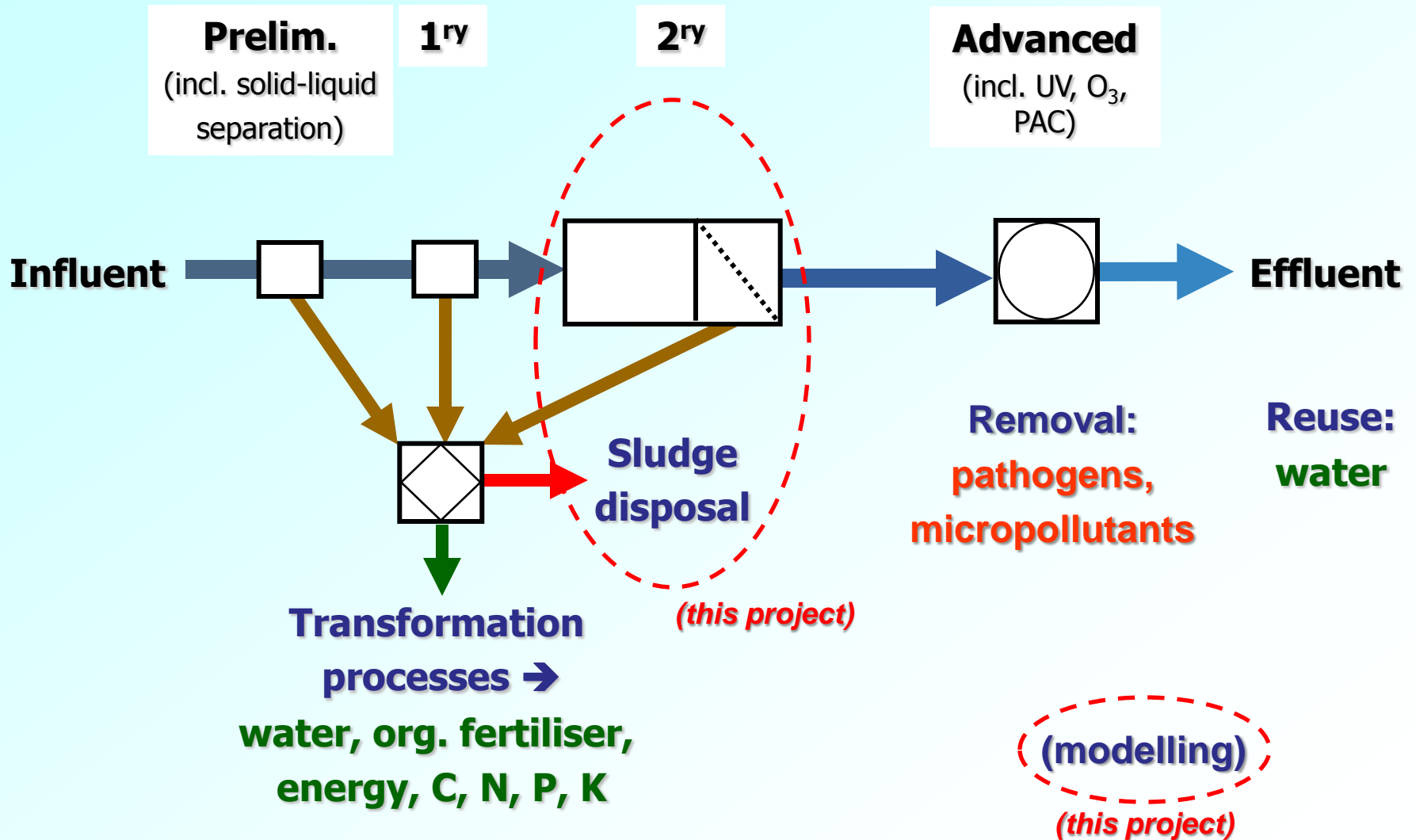
# Conclusions

- **Grit & Trash** can be removed from mixed liquor and RAS by hydrocycloning and microscreening, respectively
  - increased treatment capacity or smaller reactor size
  - effect on settling to determine
  - cost?
- $X_E$  (and probably also  $X_{U,Inf}$ ) is very slowly biodegradable under AN-OX or AN conditions

# Conclusions

- **Cannibal<sup>®</sup>**: proposed mechanisms of low sludge production:
  - main factor: long SRT (e.g. 0.40, 0.27, 0.17 g TSS/g COD at 3, 30 and 300 d SRT, respectively)
    - extra aeration costs to evaluate
  - other factors:
    - grit and trash removal by MS and HC feasible
      - MS screenings  $i_{VT} = 89 \pm 4\%$
      - about  $25 \pm 15\%$  grit removal by HC
      - not useful if there is primary treatment
      - effect on settling to determine
    - very slow biodegradation of « unbiodegradable »  
 $X_E$  and  $X_{U,Inf}$  in the bioreactor and the hypoxic fermenter  
(0.005 to 0.012 d<sup>-1</sup> for  $X_E$  at 35°C)

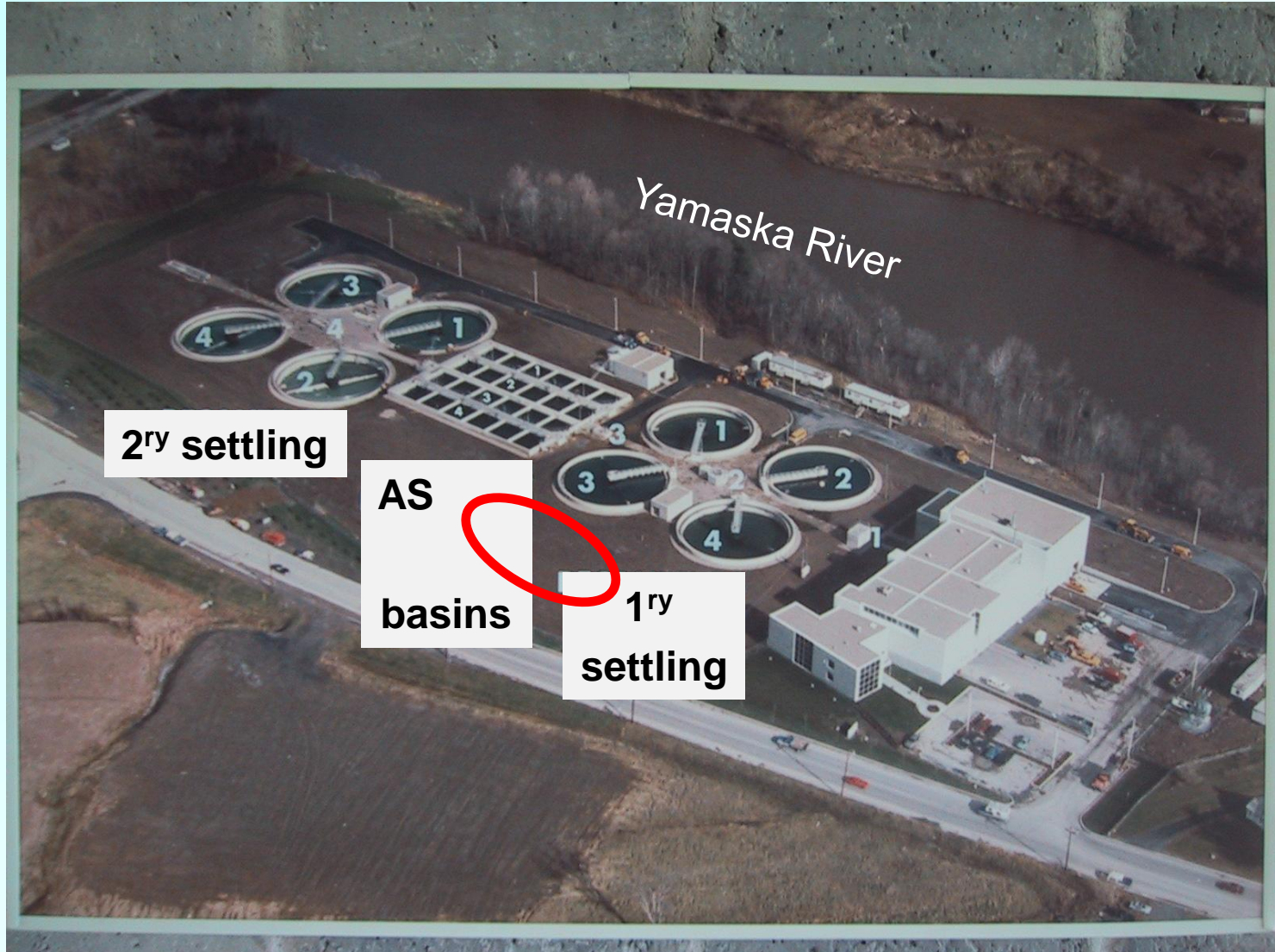
# Wastewater Treatment (or WW Resource Management)



**(to favor: energy via AD @ St-Hyac.)**

# St-Hyacinthe WWTP

## Conventional activated sludge



# St-Hyacinthe WWTP



La Presse, Feb 8, 2010

**Completely mixed LIPP anaerobic digesters (german) & drying**

**+:** energy from  $\text{CH}_4$ , sludge reduction

**-:** odors, sludge disposal, transportation GHG

**Future: agrofood waste to digest in 2 extra units**

**→  $\text{CH}_4$  for municipal vehicles**

**Future: maximize AD by bCOD recovery at 1<sup>ry</sup> (CEPT)  
and 2<sup>ry</sup> (high rate) treatment**

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- Pierre Mathieu, Robert Perry



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**Thank you for your attention**